7.0 PAVEMENT DATA

7.0 PAVEMENT DATA

7.1 General Information

A brief description of the pavement charts that follow will help in their use for airport planning. Each airplane configuration is depicted with a minimum range of six loads imposed on the main landing gear to aid in interpolation between the discrete values shown. All curves for any single chart represent data based on rated loads and tire pressures considered normal and acceptable by current aircraft tire manufacturer's standards. Tire pressures, where specifically designated on tables and charts, are at values obtained under loaded conditions as certificated for commercial use.

Section 7.2 presents basic data on the landing gear footprint configuration, maximum design taxi loads, and tire sizes and pressures.

Maximum pavement loads for certain critical conditions at the tire-to-ground interface are shown in Section 7.3, with the tires having equal loads on the struts.

Pavement requirements for commercial airplanes are customarily derived from the static analysis of loads imposed on the main landing gear struts. The chart in Section 7.4 is provided in order to determine these loads throughout the stability limits of the airplane at rest on the pavement. These main landing gear loads are used as the point of entry to the pavement design charts, interpolating load values where necessary.

The flexible pavement design curves (Section 7.5) are based on procedures set forth in Instruction Report No. S-77-1, "Procedures for Development of CBR Design Curves," dated June 1977, and as modified according to the methods described in FAA Advisory Circular AC 150/5320-6C Change 2, "Airport Pavement Design and Evaluation," dated September 14, 1988. Instruction Report No. S-77-1 was prepared by the U.S. Army Corps of Engineers Waterways Experiment Station, Soils and Pavements Laboratory, Vicksburg, Mississippi. The line showing 10,000 coverages is used to calculate Aircraft Classification Number (ACN).

The following procedure is used to develop the curves, such as shown in Section 7.5:

1. Having established the scale for pavement depth at the bottom and the scale for CBR at the top, an arbitrary line is drawn representing 6,000 annual departures.

2. Values of the aircraft gross weight are then plotted.

3. Additional annual departure lines are drawn based on the load lines of the aircraft gross weights already established.

4. An additional line representing 10,000 coverages (used to calculate the flexible pavement Aircraft Classification Number) is also placed.

All Load Classification Number (LCN) curves (Sections 7.6 and 7.8) have been developed from a computer program based on data provided in International Civil Aviation Organization (ICAO) document 9157-AN/901, Aerodrome Design Manual, Part 3, "Pavements," First Edition, 1977. LCN values are shown directly for parameters of weight on main landing gear, tire pressure, and radius of relative stiffness (ℓ) for rigid pavement or pavement thickness or depth factor (h) for flexible pavement.

Rigid pavement design curves (Section 7.7) have been prepared with the Westergaard equation in general accordance with the procedures outlined in the Design of Concrete Airport Pavement (1955 edition) by Robert G. Packard, published by the Portland Cement Association, 5420 Old Orchard Road, Skokie, Illinois 60077-1083. These curves are modified to the format described in the Portland Cement Association publication XP6705-2, Computer Program for Airport Pavement Design (Program PDILB), 1968, by Robert G. Packard.

The following procedure is used to develop the rigid pavement design curves shown in Section 7.7:

1. Having established the scale for pavement thickness to the left and the scale for allowable working stress to the right, an arbitrary load line is drawn representing the main landing gear maximum weight to be shown.

2. Values of the subgrade modulus (k) are then plotted.

3. Additional load lines for the incremental values of weight on the main landing gear are drawn on the basis of the curve for k = 300, already established.

The rigid pavement design curves (Section 7.9) have been developed based on methods used in the FAA Advisory Circular AC 150/5320-6C, September 14, 1988. The following procedure is used to develop the curves, such as shown in Section 7.9:

1. Having established the scale for pavement flexure strength on the left and temporary scale for pavement thickness on the right, an arbitrary load line is drawn representing the main landing gear maximum weight to be shown at 5,000 coverages.

2. Values of the subgrade modulus (k) are then plotted.

3. Additional load lines for the incremental values of weight are then drawn on the basis of the subgrade modulus curves already established.

4. The permanent scale for the rigid-pavement thickness is then placed. Lines for other than 5,000 coverages are established based on the aircraft pass-to-coverage ratio.

The ACN/PCN system (Section 7.10) as referenced in ICAO document 9157-AN/901, Aerodrome Design Manual, Part 3, Pavements, Second Edition 1983, provides a standardized international airplane/pavement rating system replacing the various S, T, TT, LCN, AUW, ISWL, etc., rating systems used throughout the world. ACN is the Aircraft Classification Number and PCN is the Pavement Classification Number. An aircraft having an ACN equal to or less than the PCN can operate on the pavement subject to any limitation on the tire pressure. Numerically, the ACN is two times the derived single-wheel load expressed in thousands of kilograms, where the derived single wheel load is defined as the load on a single tire inflated to 181 psi (1.25 MPa) that would have the same pavement requirements as the aircraft. Computationally, the ACN/PCN system uses the PCA program PDILB for rigid pavements and S-77-1 for flexible pavements to calculate ACN values. The method of pavement evaluation is left up to the airport with the results of their evaluation presented as follows:

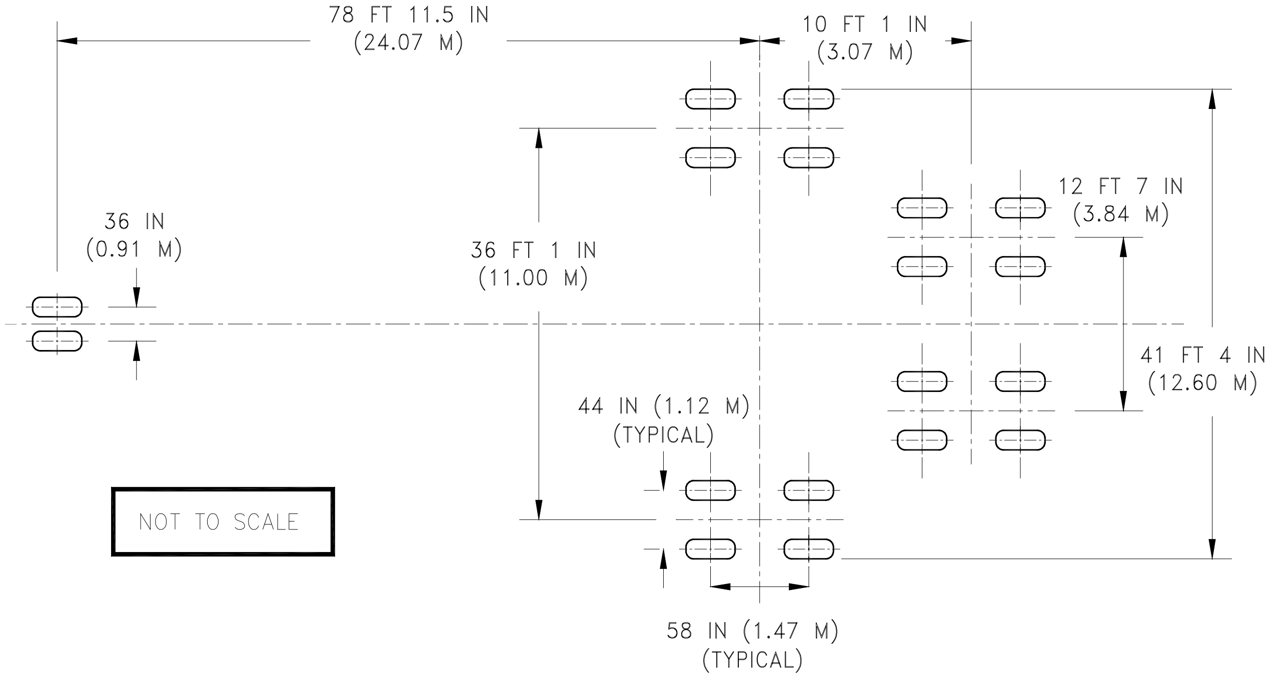
PCN	PAVEMENT TYPE	SUBGRADE CATEGORY	TIRE PRESSURE CATEGORY	EVALUATION METHOD
	R = Rigid	A = High	W = No Limit	T = Technical
	F = Flexible	B = Medium	X = To 217 psi (1.5 MPa)	U = Using Aircraft
		C = Low	Y = To 145 psi (1.0 MPa)	
		D = Ultra Low	Z = To 73 psi (0.5 MPa)	

Section 7.10.1 shows the aircraft ACN values for flexible pavements. The four subgrade categories are:

Code A - High Strength - CBR 15
Code B - Medium Strength - CBR 10
Code C - Low Strength - CBR 6
Code D - Ultra Low Strength - CBR 3

Section 7.10.2 shows the aircraft ACN values for rigid pavements. The four subgrade categories are:

Code A - High Strength, k = 550 pci (150 MN/m^3)
Code B - Medium Strength, k = 300 pci (80 MN/m^3)
Code C - Low Strength, k = 150 pci (40 MN/m^3)
Code D - Ultra Low Strength, k = 75 pci (20 MN/m^3)



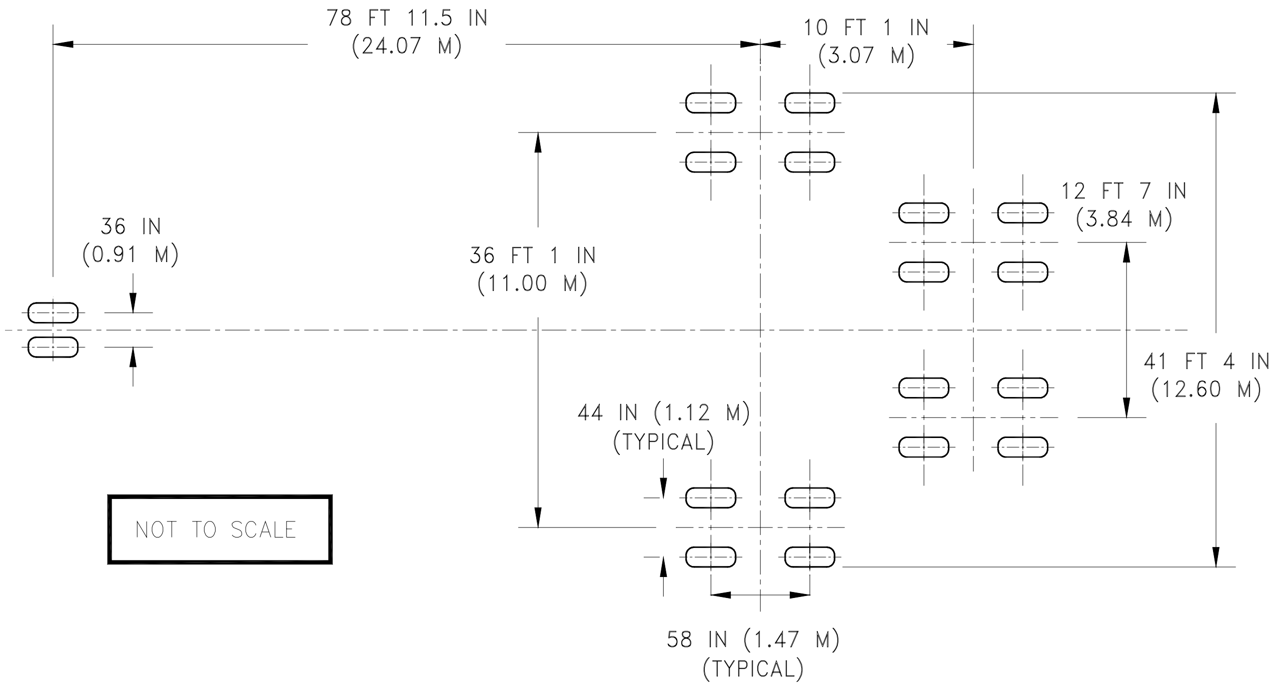
	UNITS	747-400D	747-400, 747-400COMBI		
MAXIMUM DESIGN TAXI WEIGHT	LB KG	603,000 TO 613,500 273,517 TO 278,279	803,000 364,235	836,000 TO 853,000 379,204 TO 386,915	873,000 TO 877,000 395,987 TO 397,801
PERCENT OF WEIGHT ON MAIN GEAR	%	SEE SECTION 7.4			
NOSE GEAR TIRE SIZE	IN.	49X17, 32 PR (1)	49X17, 32 PR (2)		
NOSE GEAR TIRE PRESSURE	PSI KG/CM^2	150 10.55 (1)	200 14.06 (2)		
MAIN GEAR TIRE SIZE	IN.	H49 X 19.0 - 22, 24 PR	H49 X 19.0 - 22, 32 PR		
MAIN GEAR TIRE PRESSURE (3)	PSI KG/CM^2	150 10.55	190 13.36	195 13.71	200 14.06

(1) OPTION: 49X19.0-20 32PR OR 34PR AT 150 PSI (10.55 KG/CM^2) OR H49X19.0-22, 24PR AT 150 PSI (10.55 KG/CM^2).

(2) OPTION: 49X19.0-20, 32PR OR 34PR AT 185 PSI (13.01 KG/CM2) OR H49X19.0-22, 32PR AT 175 PSI (12.30 KG/CM^2)

(3) COLD, LOADED PRESSURES SHOWN. TOLERANCE = +5/-0 PSI.

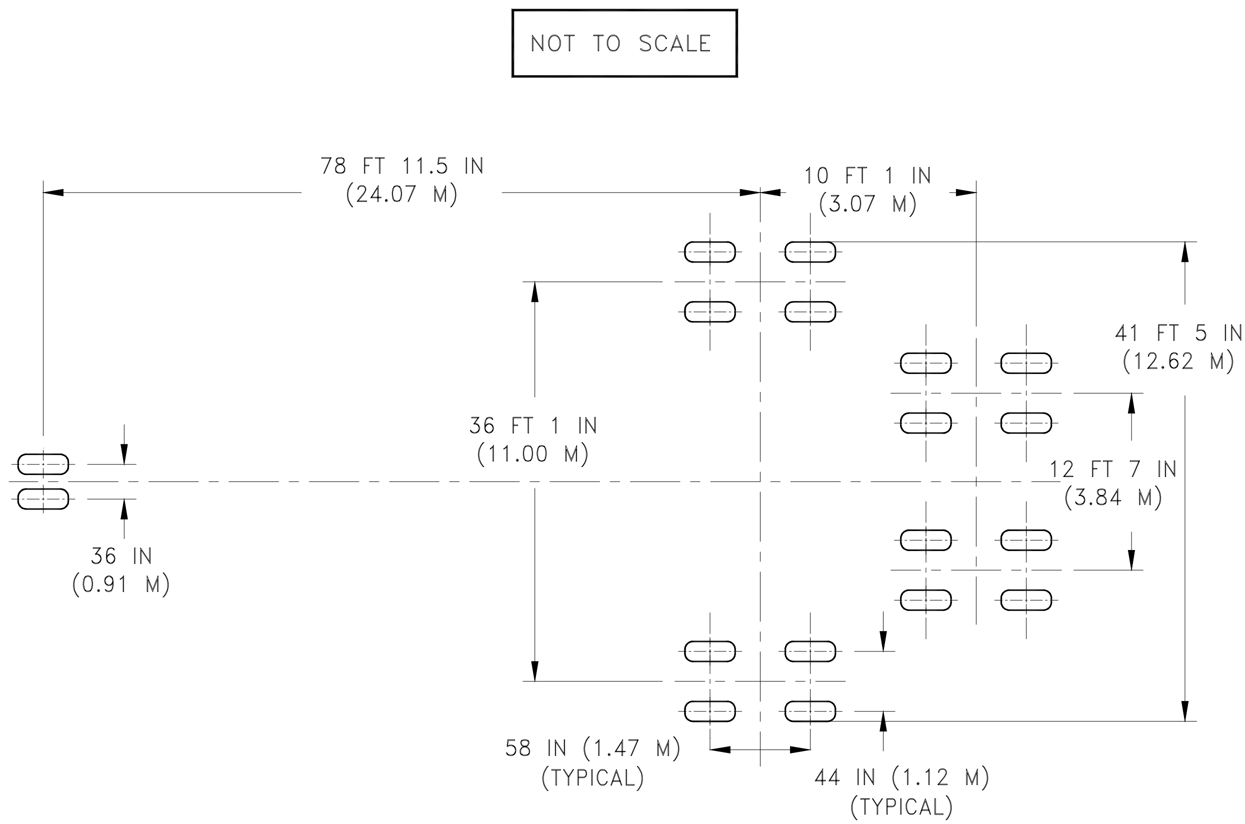
7.2.1 LANDING GEAR FOOTPRINT
MODEL 747-400, -400 COMBI, -400 DOMESTIC



	UNITS	747-400F		
MAXIMUM DESIGN TAXI WEIGHT	LB KG	803,000 364,235	836,000 TO 853,000 379,204 TO 386,915	873,000 TO 877,000 375,987 TO 397,801
PERCENT OF WEIGHT ON MAIN GEAR	%	SEE SECTION 7.4		
NOSE GEAR TIRE SIZE	IN.	H49 X 19.0 - 22 32PR		
NOSE GEAR TIRE PRESSURE	PSI KG/CM2	175 12.30		
MAIN GEAR TIRE SIZE	IN.	H49 X 19.0 - 22, 32 PR		
MAIN GEAR TIRE PRESSURE (1)	PSI KG/CM2	190 13.36	195 13.71	200 14.06

(1) COLD, LOADED PRESSURES SHOWN. TOLERANCE = +5/-0 PSI.

7.2.2 LANDING GEAR FOOTPRINT
MODEL 747-400 FREIGHTER

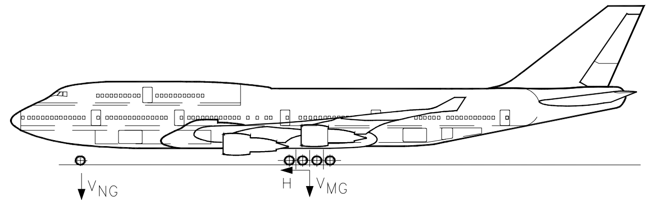


	UNITS	747-400ER	747-400ER FREIGHTER
MAXIMUM DESIGN TAXI WEIGHT	LB KG	913,000 414,130	913,000 414,130
PERCENT OF WEIGHT ON MAIN GEAR	%	SEE SECTION 7.4	
NOSE GEAR TIRE SIZE	IN.	50 X 20.0 R 22, 34 PR	50 X 20.0 R22, 34 PR
NOSE GEAR TIRE PRESSURE	PSI KG/CM^2	190 13.36	190 13.36
MAIN GEAR TIRE SIZE	IN.	50 X 20.0 R 22, 34 PR	50 X 20.0 R, 34 PR
MAIN GEAR TIRE PRESSURE	PSI KG/CM^2	230 16.17	230 16.17

7.2.3 LANDING GEAR FOOTPRINT
MODEL 747-400ER, -400ER FREIGHTER

V_{NG} = MAXIMUM VERTICAL NOSE GEAR GROUND LOAD AT MOST FORWARD CENTER OF GRAVITY
V_{MG} = MAXIMUM VERTICAL MAIN GEAR GROUND LOAD AT MOST AFT CENTER OF GRAVITY
H = MAXIMUM HORIZONTAL GROUND LOAD FROM BRAKING

NOTES: 1. ALL LOADS CALCULATED USING AIRPLANE MAXIMUM DESIGN TAXI WEIGHT
2. ALL CALCULATED VALUES AND CONVERSIONS ROUNDED TO NEAREST 100 LB AND 50 KG.

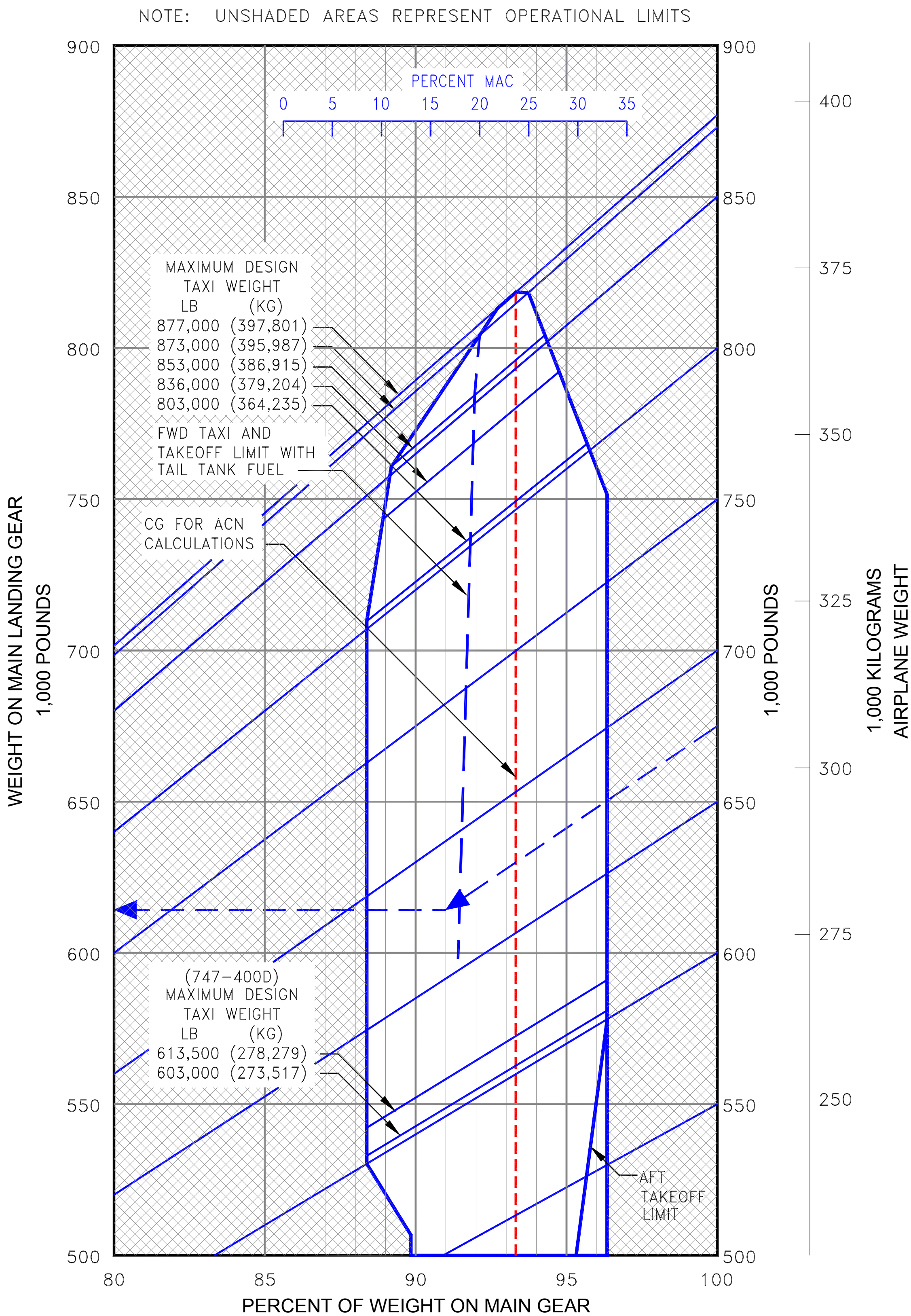


AIRPLANE MODEL	UNITS	MAX DESIGN TAXI WEIGHT	V_{NG}		V_{MG} PER STRUT (4)	H PER STRUT (4)	
			STATIC AT MOST FWD C.G.	STATIC + BRAKING 10 FT/SEC^2 DECEL	MAX LOAD AT STATIC AFT C.G.	STEADY BRAKING 10 FT/SEC^2 DECEL	AT INSTANTANEOUS BRAKING (μ = 0.8)
747-400	LB	803,000	93,300	138,200	191,500	62,300	153,200
	KG	364,250	42,350	62,700	86,850	28,300	69,500
747-400*	LB	803,000	65,900	110,800	191,500	62,300	153,200
	KG	364,250	29,900	50,250	86,850	28,300	69,500
747-400	LB	836,000	93,000	139,900	197,300	64,900	157,800
	KG	379,200	42,200	63,450	89,500	29,450	71,600
747-400*	LB	836,000	68,100	114,800	197,300	64,900	157,800
	KG	379,200	30,850	52,100	89,500	29,450	71,600
747-400	LB	853,000	92,200	139,900	200,300	66,200	160,200
	KG	386,900	41,800	63,450	90,850	30,050	72,650
747-400*	LB	853,000	68,600	116,300	200,300	66,200	160,200
	KG	386,900	31,100	52,750	90,850	30,050	72,650
747-400	LB	873,000	68,800	117,700	204,500	67,800	163,600
	KG	396,000	31,200	53,400	92,750	30,750	74,200
747-400	LB	877,000	64,000	114,000	204,600	68,100	163,700
	KG	397,800	29,000	51,700	92,800	30,900	74,250
747-400F	LB	873,000	80,100	116,200	204,500	67,800	163,600
	KG	396,000	36,350	52,700	92,750	30,750	74,200
747-400F*	LB	873,000	67,400	116,200	204,500	67,800	163,600
	KG	396,000	30,550	52,700	92,750	30,750	74,200
747-400F	LB	877,000	76,500	127,900	204,600	68,100	163,700
	KG	397,800	34,700	58,000	92,800	30,900	74,250
747-400F*	LB	877,000	67,400	118,800	204,600	68,100	163,700
	KG	397,800	30,550	53,900	92,800	30,900	74,250
747-400D	LB	603,000	70,100	103,800	145,200	46,800	116,200
	KG	273,500	31,800	47,100	65,900	21,250	52,700
747-400D	LB	613,500	71,300	105,600	147,800	47,600	118,200
	KG	278,300	32,350	47,900	67,050	21,600	53,600
747-400ER	LB	913,000	71,950	122,400	213,600	70,900	170,900
	KG	414,150	32,650	55,550	96,900	32,150	77,500
747-400ER FREIGHTER	LB	913,000	77,300	130,950	213,600	70,900	170,900
	KG	414,150	35,050	59,400	96,900	32,150	77,500

* AIRPLANE WITH TAIL TANK FUEL

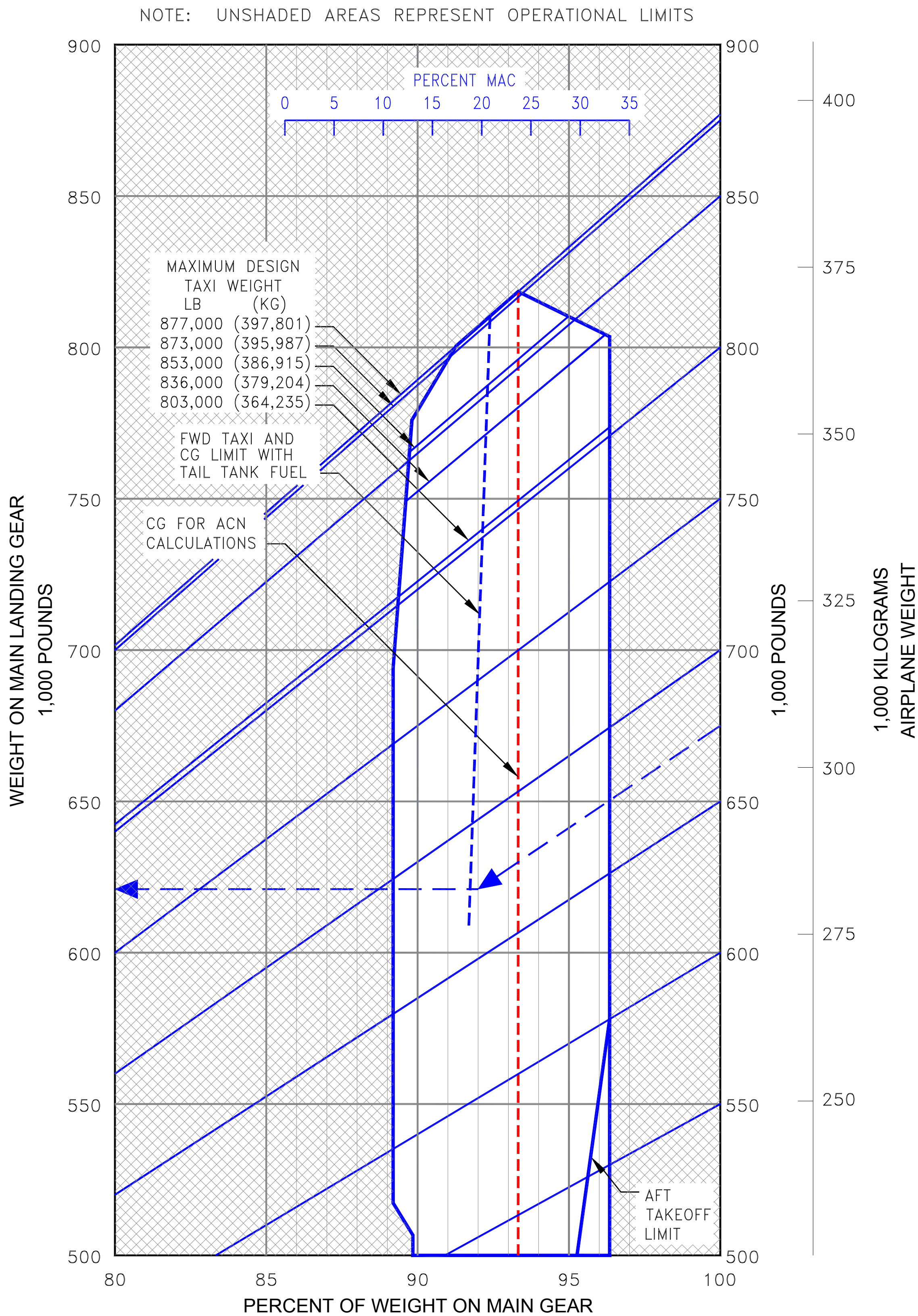
7.3. MAXIMUM PAVEMENT LOADS

MODEL 747-400

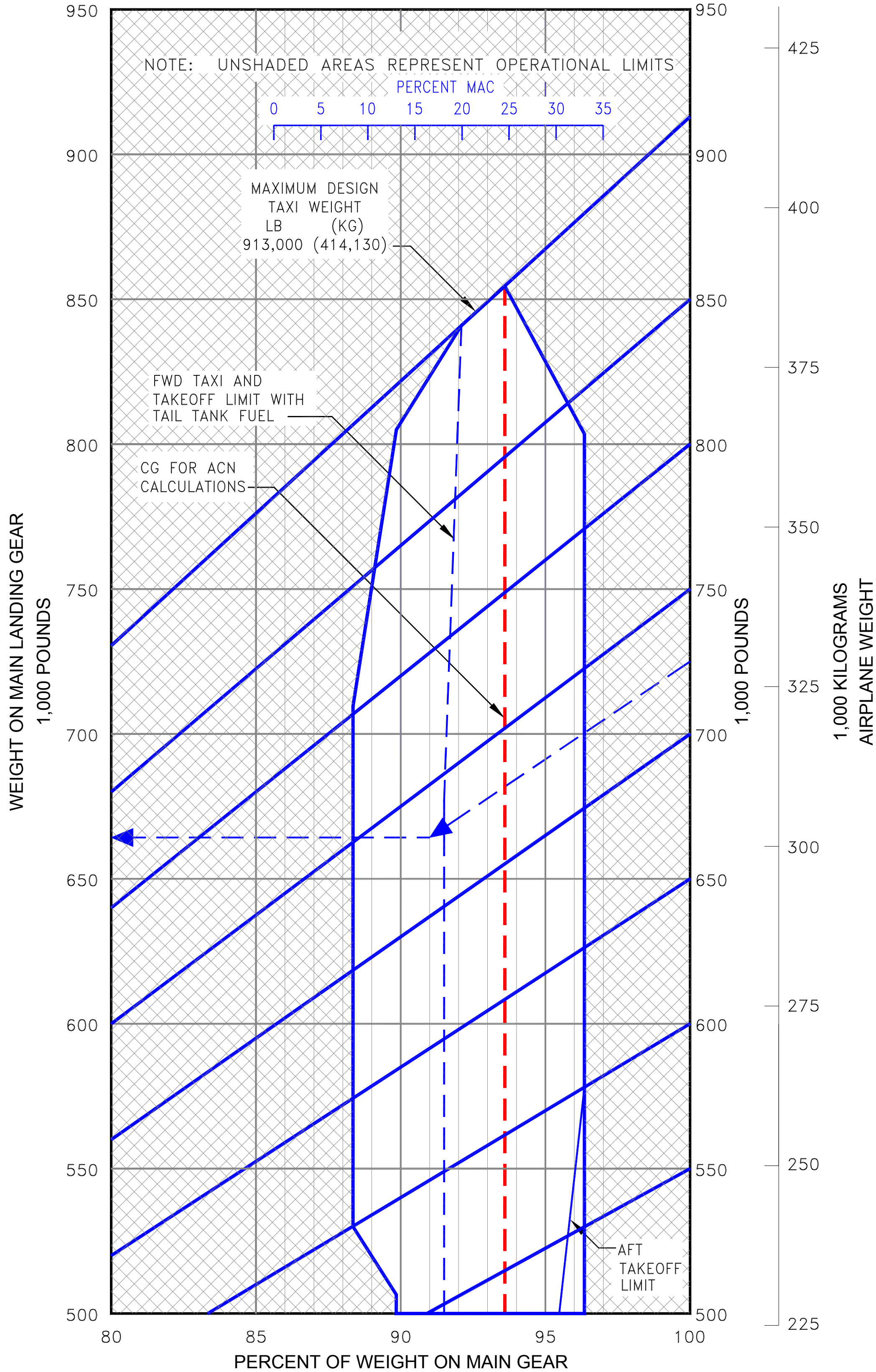


7.4.1 LANDING GEAR LOADING ON PAVEMENT

MODEL 747-400, -400 COMBI, -400 DOMESTIC

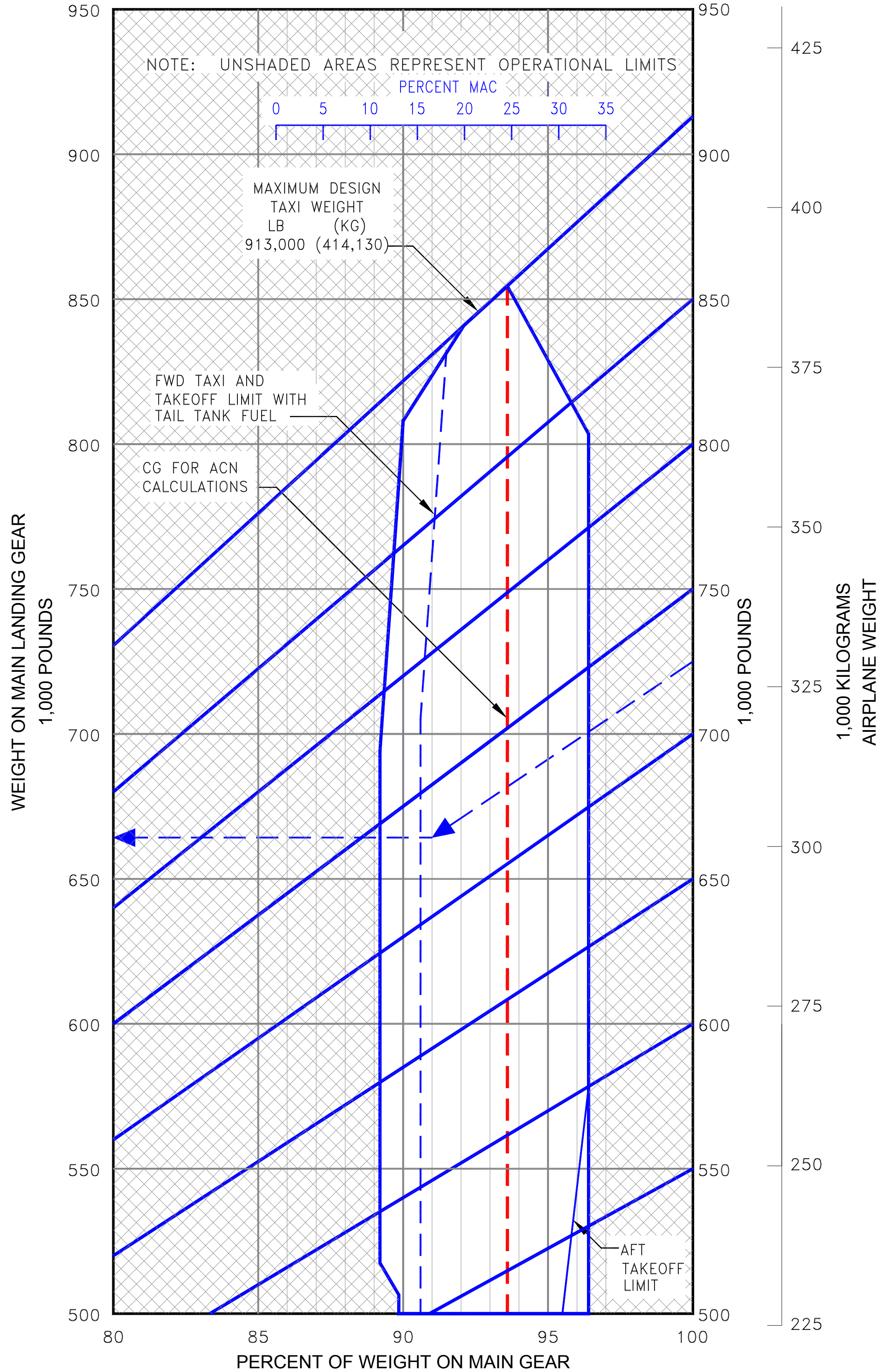


7.4.2 LANDING GEAR LOADING ON PAVEMENT
MODEL 747-400 FREIGHTER



7.4.3 LANDING GEAR LOADING ON PAVEMENT

MODEL 747-400ER



7.4.4 LANDING GEAR LOADING ON PAVEMENT

MODEL 747-400ER FREIGHTER

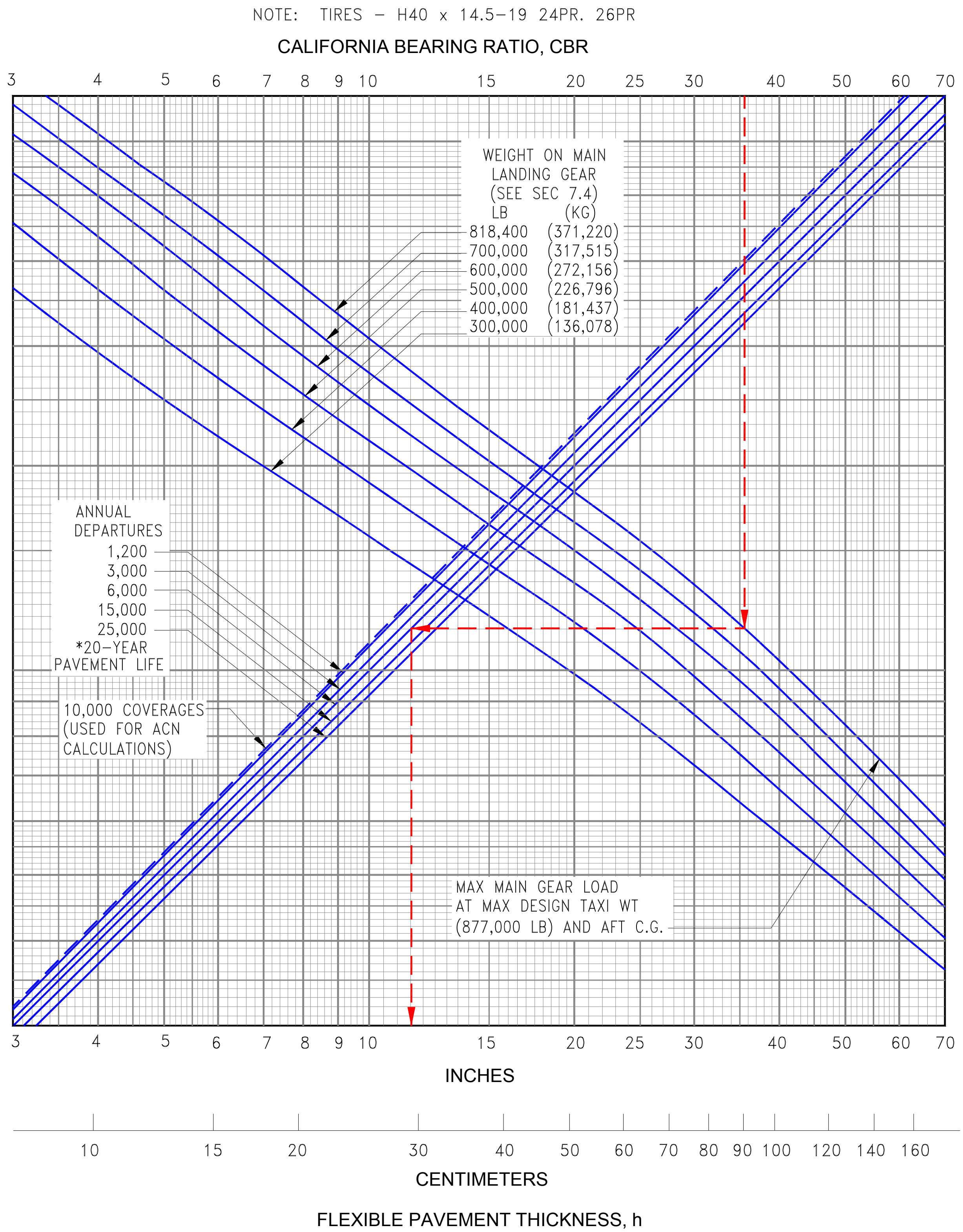
7.5 Flexible Pavement Requirements - U.S. Army Corps of Engineers Method (S-77-1) and FAA Design Method

The following flexible-pavement design chart presents the data of six incremental main-gear loads at the minimum tire pressure required at the maximum design taxi weight.

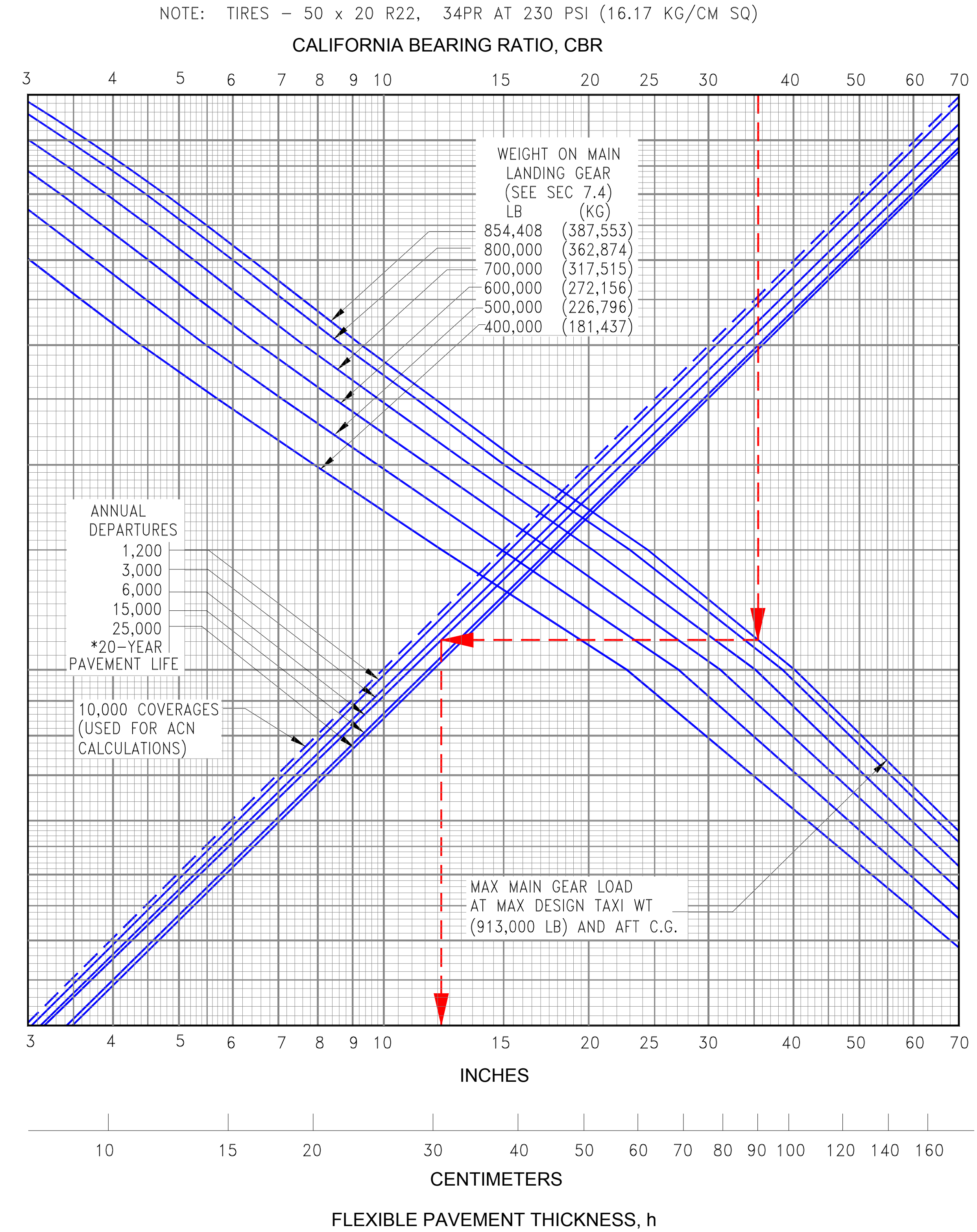
In the example shown in Section 7.5.1, for a CBR of 35.5 and an annual departure level of 6,000, the required flexible pavement thickness for a 747-400 airplane with a main gear loading of 818,400 pounds is 13.1 inches. In Section 7.5.2, for the same CBR and departure levels, the required flexible pavement thickness for a 747-400ER airplane with a main gear loading of 854,408 pounds is 14.2 inches.

The line showing 10,000 coverages is used for ACN calculations (see Section 7.10).

The FAA design method uses a similar procedure using total airplane weight instead of weight on the main landing gears. The equivalent main gear loads for a given airplane weight could be calculated from Section 7.4.



7.5.1 FLEXIBLE PAVEMENT REQUIREMENTS - U.S. ARMY CORPS OF ENGINEERS DESIGN METHOD (S-77-1) AND FAA DESIGN METHOD
MODEL 747-400, -400 COMBI, -400 DOMESTIC, - 400 FREIGHTER



7.5.2 FLEXIBLE PAVEMENT REQUIREMENTS - U.S. ARMY CORPS OF ENGINEERS DESIGN METHOD (S-77-1)

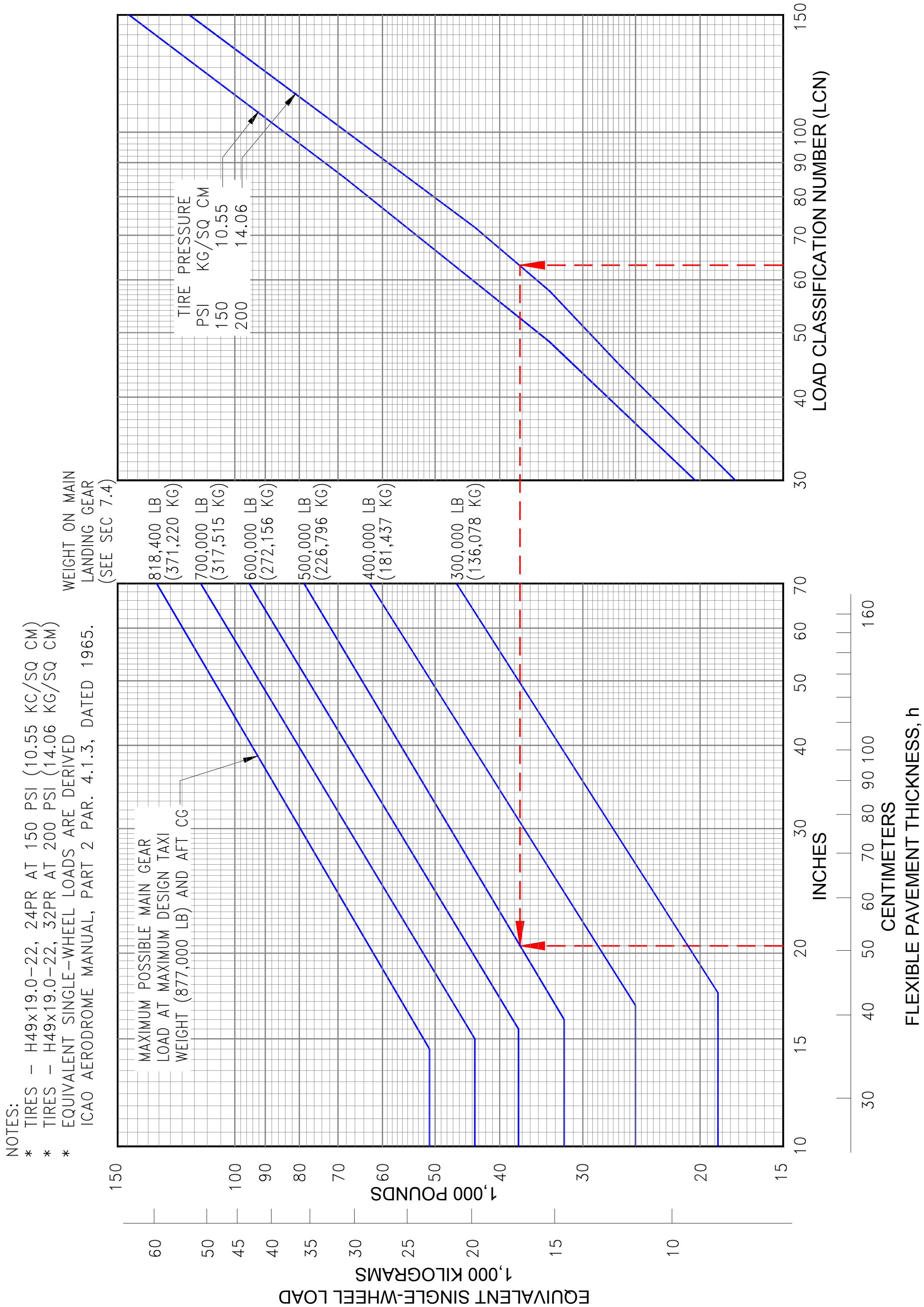
MODEL 747-400ER, -400ER FREIGHTER

7.6 Flexible Pavement Requirements - LCN Method

To determine the airplane weight that can be accommodated on a particular flexible pavement, both the Load Classification Number (LCN) of the pavement and the thickness must be known.

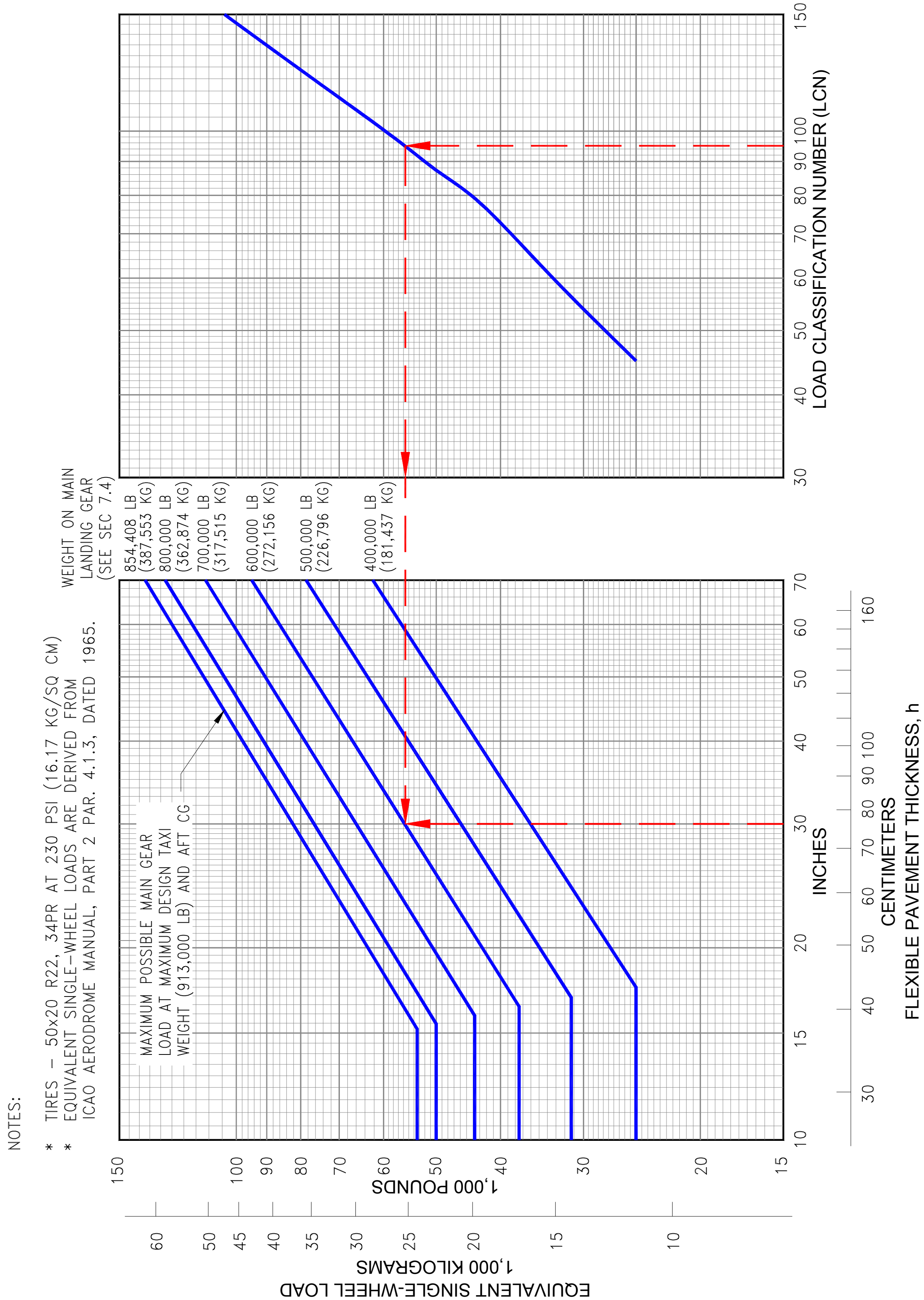
In the example shown in Section 7.6.1, flexible pavement thickness is shown at 21 inches with an LCN of 63. For these conditions, the apparent maximum allowable weight permissible on the main landing gear is 500,000 pounds for a 747-400 airplane with 200-psi main gear tires. In Section 7.6.2, for a flexible pavement thickness of 30 inches with an LCN of 95, the apparent maximum allowable weight permissible on the main landing gear is 600,000 pounds for a 747-400ER airplane with 230-psi main gear tires

Note: If the resultant aircraft LCN is not more that 10% above the published pavement LCN, the bearing strength of the pavement can be considered sufficient for unlimited use by the airplane. The figure 10% has been chosen as representing the lowest degree of variation in LCN that is significant (reference: ICAO Aerodrome Design Manual, Part 3, "Pavements,", First Edition dated 1977.)



7.6.1 FLEXIBLE PAVEMENT REQUIREMENTS - LCN METHOD

MODEL 747-400, -400 COMBI, -400 DOMESTIC, - 400 FREIGHTER



7.6.2 FLEXIBLE PAVEMENT REQUIREMENTS - LCN METHOD

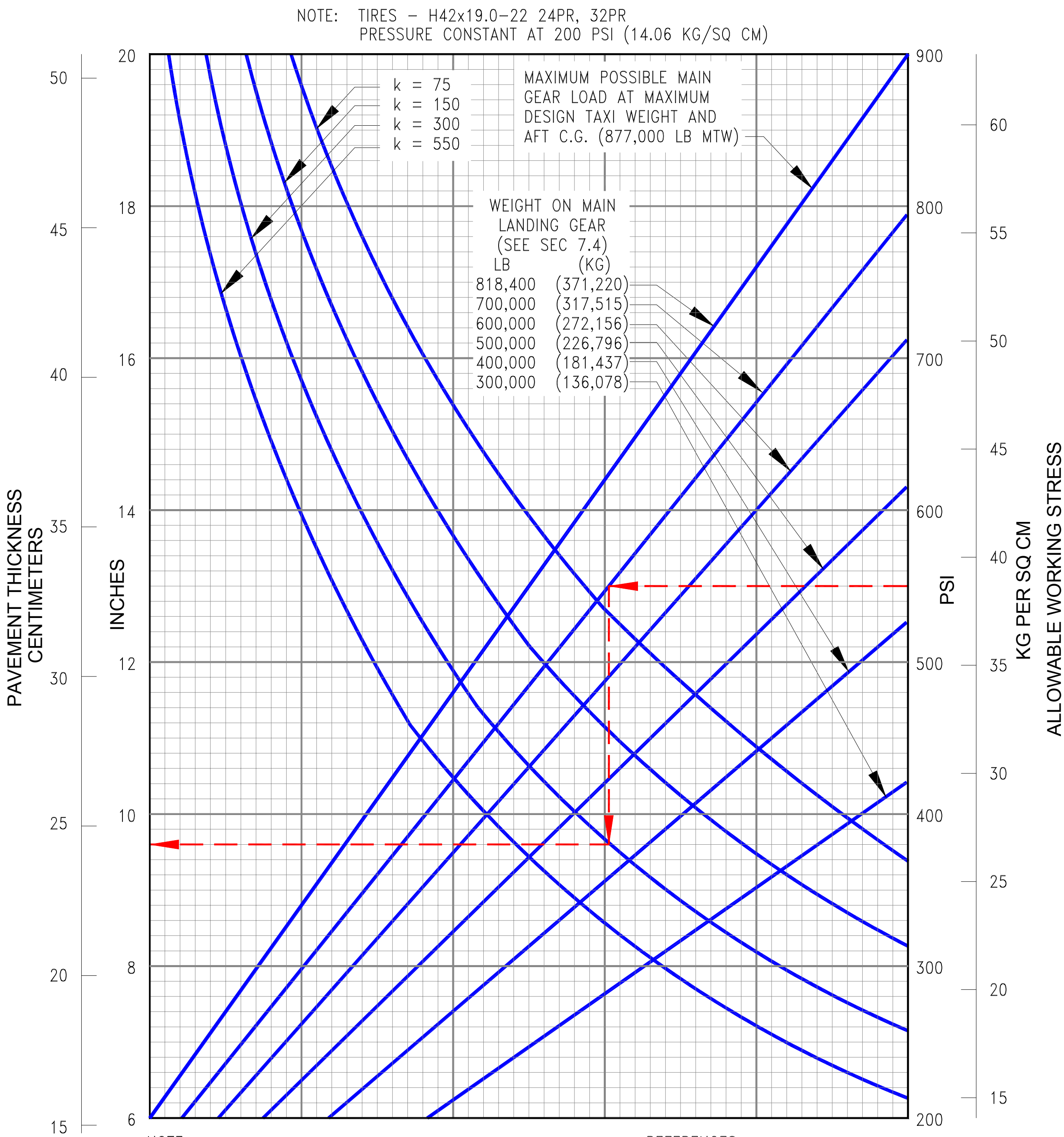
MODEL 747-400ER, -400ER FREIGHTER

7.7 Rigid Pavement Requirements - Portland Cement Association Design Method

The Portland Cement Association method of calculating rigid pavement requirements is based on the computerized version of "Design of Concrete Airport Pavement" (Portland Cement Association, 1965) as described in XP6705-2, "Computer Program for Airport Pavement Design" by Robert G. Packard, Portland Cement Association, 1968.

The rigid pavement design charts in Section 7.7.1 and Section 7.7.2 present data for six incremental main gear loads at the minimum tire pressure required at the maximum design taxi weight.

In the example shown in Section 7.7.1, for an allowable working stress of 550 psi, a main gear load on a 747-400 airplane of 700,000 pounds, and a subgrade strength (k) of 300, the required rigid pavement thickness is 9.6 inches. In Section 7.7.2, for an allowable working stress of 550 psi, a main gear load on a 747-400ER airplane of 800,000 pounds, and a subgrade strength (k) of 300, the required rigid pavement thickness is 10.8 inches.

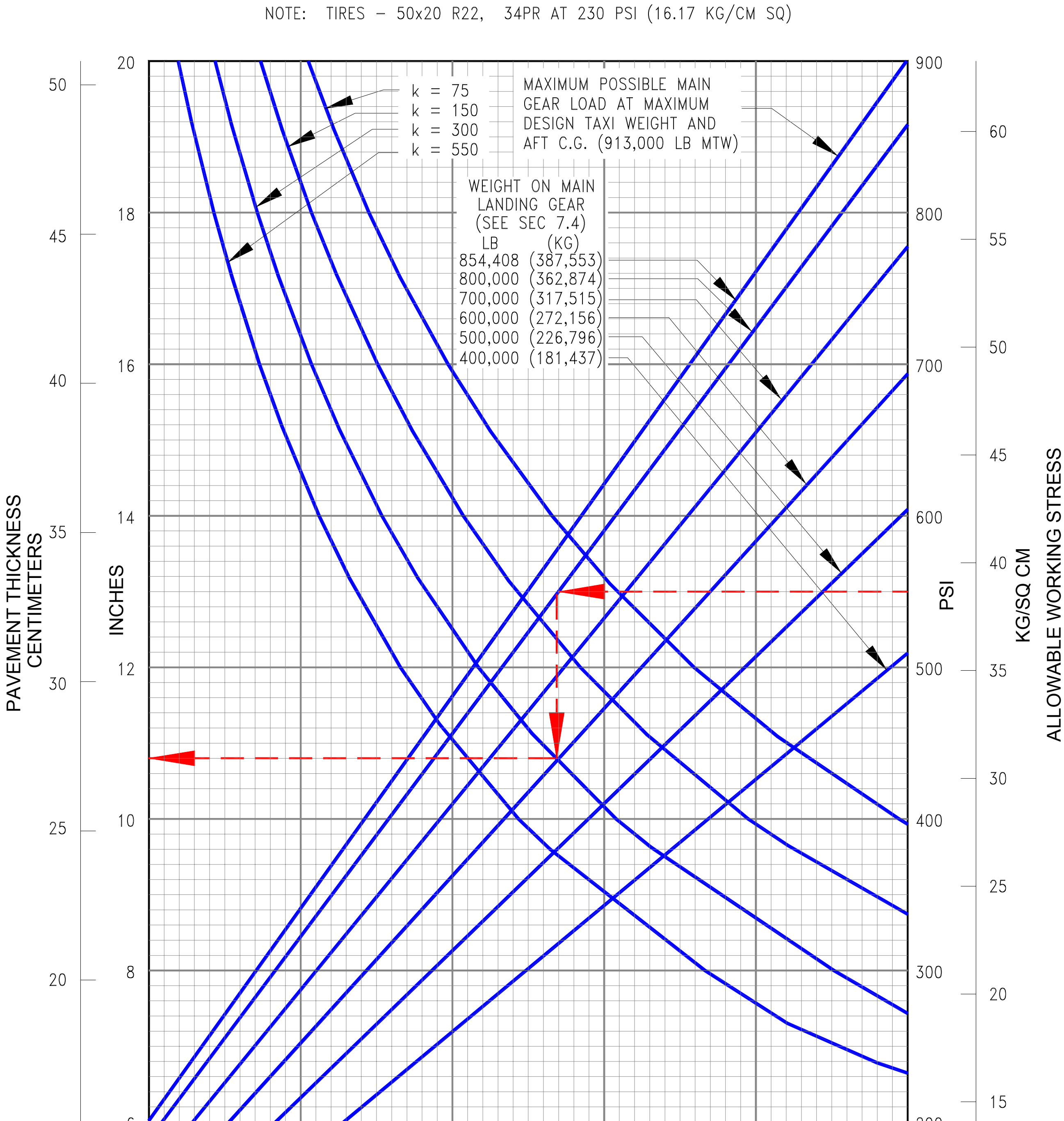


NOTE:
THE VALUES OBTAINED BY USING THE MAXIMUM LOAD REFERENCE LINE AND ANY VALUE OF k ARE EXACT.
FOR LOADS LESS THAN MAXIMUM, THE CURVES ARE EXACT FOR k = 300 BUT DEVIATE SLIGHTLY FOR OTHER VALUES OF k.

REFERENCES:
"DESIGN OF CONCRETE AIRPORT PAVEMENT" AND "COMPUTER PROGRAM FOR AIRPORT PAVEMENT DESIGN - PROGRAM PDILB" PORTLAND CEMENT ASSOCIATION.

7.7.1 RIGID PAVEMENT REQUIREMENTS - PORTLAND CEMENT ASSOCIATION DESIGN METHOD

MODEL 747-400, -400 COMBI, -400 DOMESTIC, - 400 FREIGHTER



NOTE:
THE VALUES OBTAINED BY USING THE MAXIMUM LOAD REFERENCE LINE AND ANY VALUE OF k ARE EXACT.
FOR LOADS LESS THAN MAXIMUM, THE CURVES ARE EXACT FOR k = 300 BUT DEVIATE SLIGHTLY FOR OTHER VALUES OF k.

REFERENCES:
"DESIGN OF CONCRETE AIRPORT PAVEMENT" AND "COMPUTER PROGRAM FOR AIRPORT PAVEMENT DESIGN - PROGRAM PDILB" PORTLAND CEMENT ASSOCIATION.

7.7.2 RIGID PAVEMENT REQUIREMENTS - PORTLAND CEMENT ASSOCIATION DESIGN METHOD

MODEL 747-400ER, -400ER FREIGHTER

7.8 Rigid Pavement Requirements - LCN Conversion

To determine the airplane weight that can be accommodated on a particular rigid pavement, both the LCN of the pavement and the radius of relative stiffness (ℓ) of the pavement must be known.

In the example shown in Section 7.8.2, for a rigid pavement with a radius of relative stiffness of 48 with an LCN of 58, the apparent maximum allowable weight permissible on the main landing gear is 400,000 pounds for a 747-400 airplane with 200-psi main tires. In Section 7.8.3, for a rigid pavement with a radius of relative stiffness of 47 with an LCN of 91, the apparent maximum allowable weight permissible on the main landing gear is 600,000 pounds for a 747-400ER airplane with 230-psi main tires.

Note: If the resultant aircraft LCN is not more that 10% above the published pavement LCN, the bearing strength of the pavement can be considered sufficient for unlimited use by the airplane. The figure 10% has been chosen as representing the lowest degree of variation in LCN that is significant (reference: ICAO Aerodrome Design Manual, Part 3, "Pavements," First Edition dated 1977).

RADIUS OF RELATIVE STIFFNESS (ℓ)

VALUES IN INCHES

$$\ell = \sqrt[4]{\frac{Ed^3}{12(1-\mu^2)k}} = 24.1652\sqrt[4]{\frac{d^3}{k}}$$

WHERE: E = YOUNG'S MODULUS OF ELASTICITY = 4 x 10^6 psi

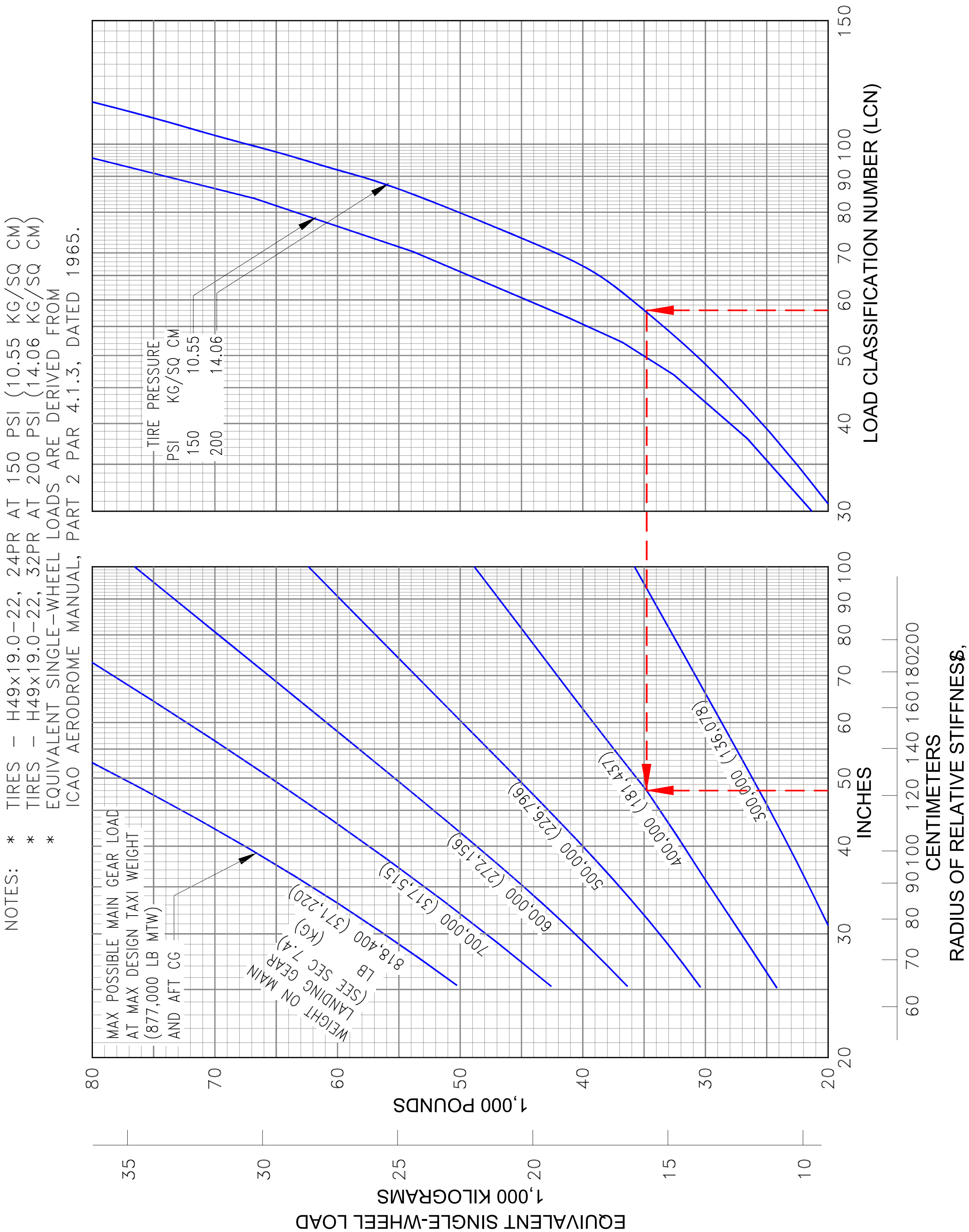
k = SUBGRADE MODULUS, LB PER CU IN

d = RIGID PAVEMENT THICKNESS, IN

μ = POISSON'S RATIO = 0.15

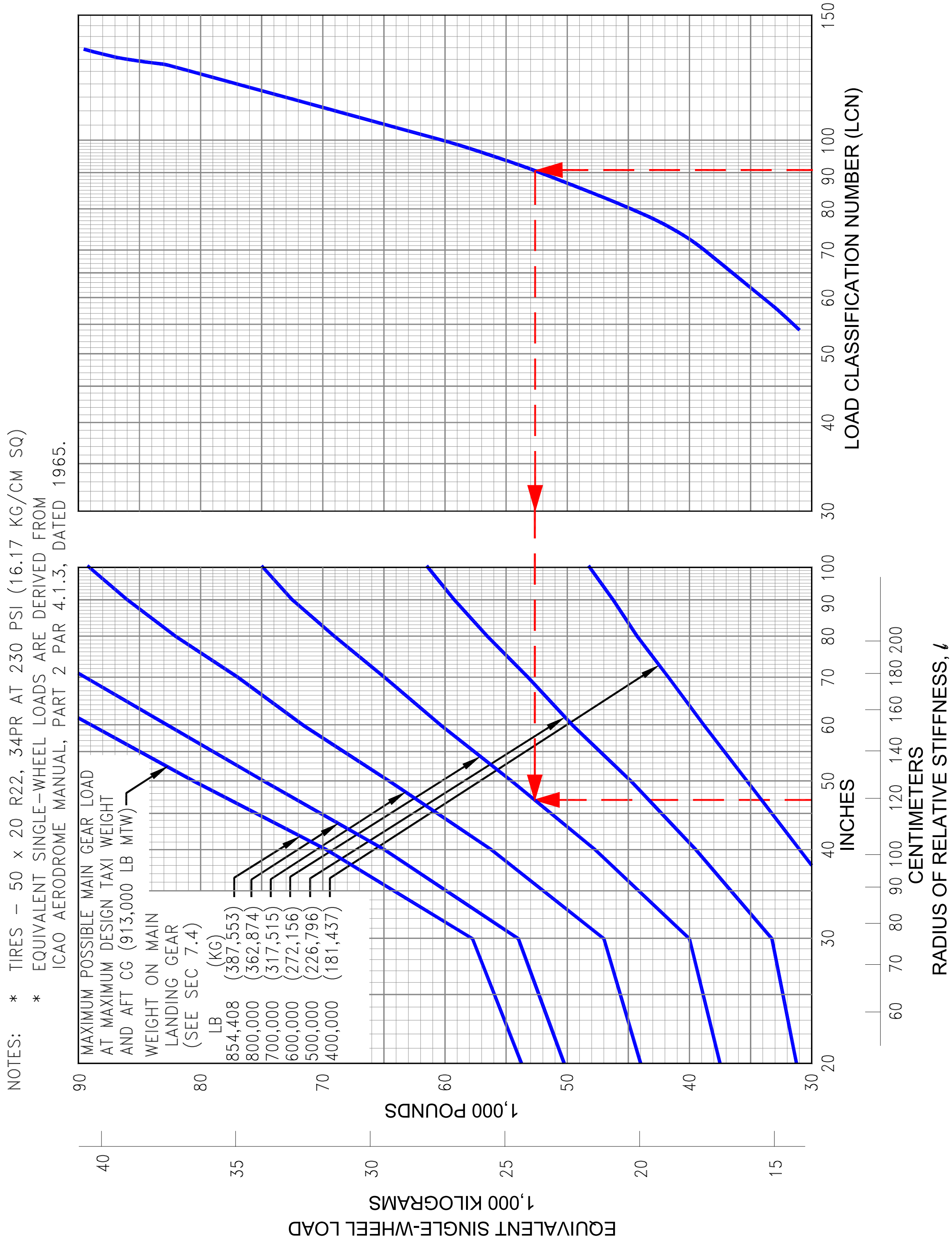
d	k = 75	k = 100	k = 150	k = 200	k = 250	k = 300	k = 350	k = 400	k = 500	k = 550
6.0	31.48	29.29	26.47	24.63	23.30	22.26	21.42	20.71	19.59	19.13
6.5	33.42	31.10	28.11	26.16	24.74	23.63	22.74	21.99	20.80	20.31
7.0	35.33	32.88	29.71	27.65	26.15	24.99	24.04	23.25	21.99	21.47
7.5	37.21	34.63	31.29	29.12	27.54	26.31	25.32	24.49	23.16	22.61
8.0	39.06	36.35	32.84	30.56	28.91	27.62	26.57	25.70	24.31	23.73
8.5	40.87	38.04	34.37	31.99	30.25	28.90	27.81	26.90	25.44	24.84
9.0	42.66	39.70	35.88	33.39	31.57	30.17	29.03	28.07	26.55	25.93
9.5	44.43	41.35	37.36	34.77	32.88	31.42	30.23	29.24	27.65	27.00
10.0	46.17	42.97	38.83	36.13	34.17	32.65	31.41	30.38	28.73	28.06
10.5	47.89	44.57	40.27	37.48	35.44	33.87	32.58	31.52	29.81	29.10
11.0	49.59	46.15	41.70	38.81	36.70	35.07	33.74	32.63	30.86	30.14
11.5	51.27	47.72	43.12	40.12	37.95	36.26	34.89	33.74	31.91	31.16
12.0	52.94	49.26	44.51	41.43	39.18	37.43	36.02	34.83	32.94	32.17
12.5	54.58	50.80	45.90	42.71	40.40	38.60	37.14	35.92	33.97	33.17
13.0	56.21	52.31	47.27	43.99	41.60	39.75	38.25	36.99	34.98	34.16
13.5	57.83	53.81	48.63	45.25	42.80	40.89	39.34	38.05	35.99	35.14
14.0	59.43	55.30	49.97	46.50	43.98	42.02	40.43	39.10	36.98	36.11
14.5	61.01	56.78	51.30	47.74	45.15	43.14	41.51	40.15	37.97	37.07
15.0	62.58	58.24	52.62	48.97	46.32	44.25	42.58	41.18	38.95	38.03
15.5	64.14	59.69	53.93	50.19	47.47	45.35	43.64	42.21	39.92	38.98
16.0	65.69	61.13	55.23	51.40	48.61	46.45	44.69	43.22	40.88	39.92
16.5	67.22	62.55	56.52	52.60	49.75	47.53	45.73	44.23	41.83	40.85
17.0	68.74	63.97	57.80	53.79	50.87	48.61	46.77	45.23	42.78	41.77
17.5	70.25	65.38	59.07	54.97	51.99	49.68	47.80	46.23	43.72	42.69
18.0	71.75	66.77	60.34	56.15	53.10	50.74	48.82	47.22	44.65	43.60
19.0	74.72	69.54	62.83	58.47	55.30	52.84	50.84	49.17	46.50	45.41
20.0	77.65	72.26	65.30	60.77	57.47	54.91	52.83	51.10	48.33	47.19
21.0	80.55	74.96	67.73	63.03	59.61	56.95	54.80	53.00	50.13	48.95
22.0	83.41	77.62	70.14	65.27	61.73	58.98	56.75	54.88	51.91	50.68
23.0	86.23	80.25	72.51	67.48	63.82	60.98	58.67	56.74	53.67	52.40
24.0	89.03	82.85	74.86	69.67	65.89	62.95	60.57	58.58	55.41	54.10
25.0	91.80	85.43	77.19	71.84	67.94	64.91	62.46	60.41	57.13	55.78

7.8.1 RADIUS OF RELATIVE STIFFNESS (REFERENCE: PORTLAND CEMENT ASSOCIATION)



7.8.2 RIGID PAVEMENT REQUIREMENTS - LCN CONVERSION

MODEL 747-400, -400 COMBI, -400 DOMESTIC, - 400 FREIGHTER



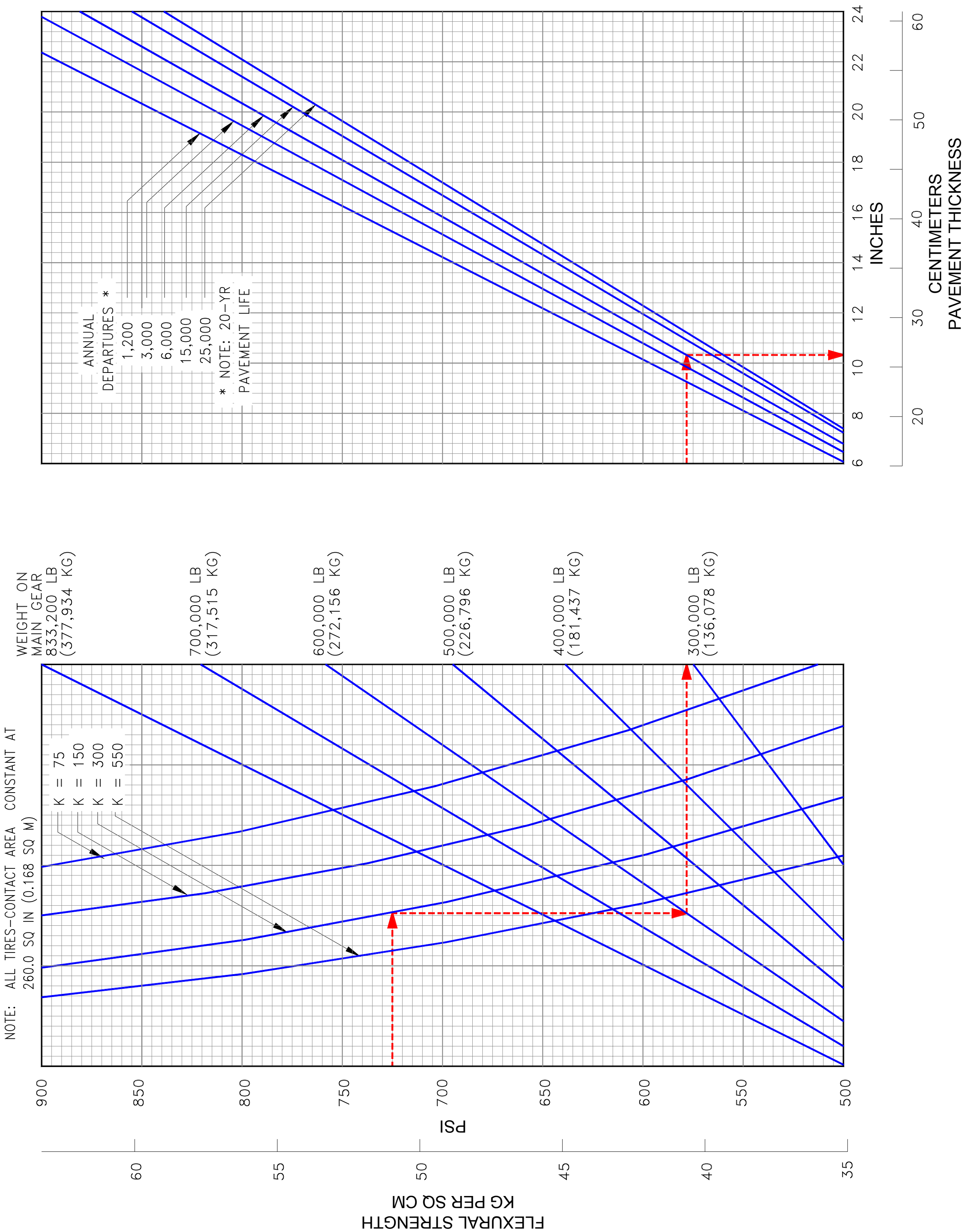
7.8.3 RIGID PAVEMENT REQUIREMENTS - LCN CONVERSION

MODEL 747-400ER, -400ER FREIGHTER

7.9 Rigid Pavement Requirements - FAA Design Method

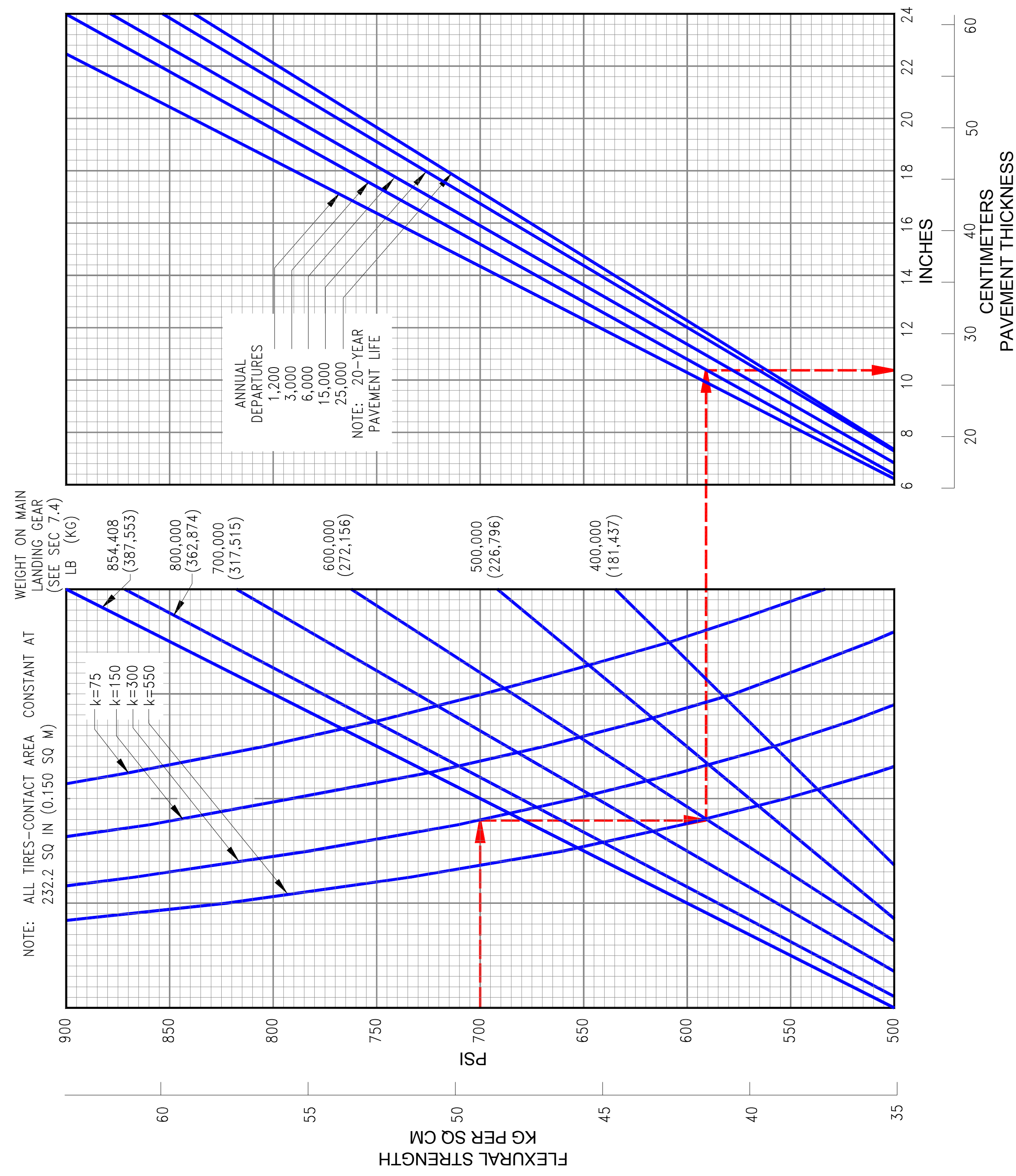
The rigid pavement design charts shown in Section 7.9.1 and Section 7.9.2 present data on six incremental main gear loads at the minimum tire pressure required at the maximum design taxi weight.

In the example shown in Section 7.9.1, for a pavement flexure strength of 725 psi, a subgrade strength of k = 300, and an annual departure level of 6,000, the required rigid pavement thickness for a 747-400 airplane with a main gear load of 600,000 pounds is 10.4 inches. In Section 7.9.2, for a pavement flexure strength of 700 psi, a subgrade strength of k = 300, and an annual departure level of 3,000, the required rigid pavement thickness for a 747-40ER airplane with a main gear load of 600,000 pounds is 10.4 inches.



7.9.1 RIGID PAVEMENT REQUIREMENTS - FAA DESIGN METHOD

MODEL 747-400, -400 COMBI, -400 DOMESTIC, - 400 FREIGHTER



7.9.2 RIGID PAVEMENT REQUIREMENTS - FAA DESIGN METHOD

MODEL 747-400ER, -400ER FREIGHTER

7.10 ACN/PCN Reporting System: Flexible and Rigid Pavements

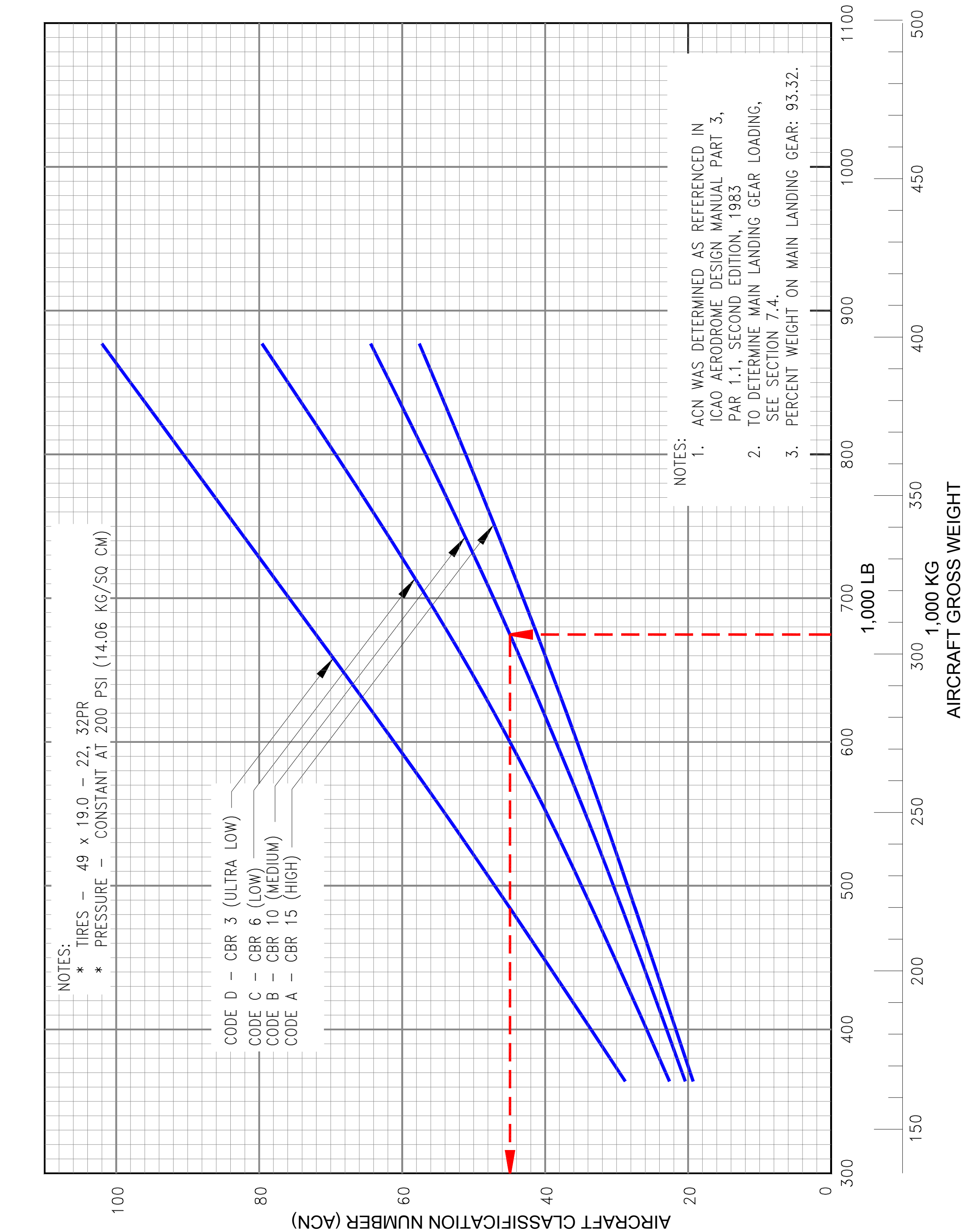
To determine the ACN of an aircraft on flexible or rigid pavement, both the aircraft gross weight and the subgrade strength category must be known. In the example in Section 7.10.1, for a 747-400 aircraft with a gross weight of 675,000 pounds and medium subgrade strength, the flexible pavement ACN is 45. In Section 7.10.3, for the same aircraft and subgrade strength, the rigid pavement ACN is 43.8. In Section 7.10.2, for a 747-400ER aircraft with a gross weight of 900,000 pounds and medium subgrade strength, the flexible pavement ACN is 60.5. In Section 7.10.4, for the same aircraft and subgrade strength, the rigid pavement ACN is 57.8.

Notes: 1. An aircraft with an ACN equal to or less that the reported PCN can operate on that pavement subject to any limitations on the tire pressure. (Ref: ICAO Annex 14 Aerodromes, First Edition, July 1990.)

2. The ACN values on the Flexible Pavement charts were calculated using alpha factors proposed by the ICAO ACN Study Group.

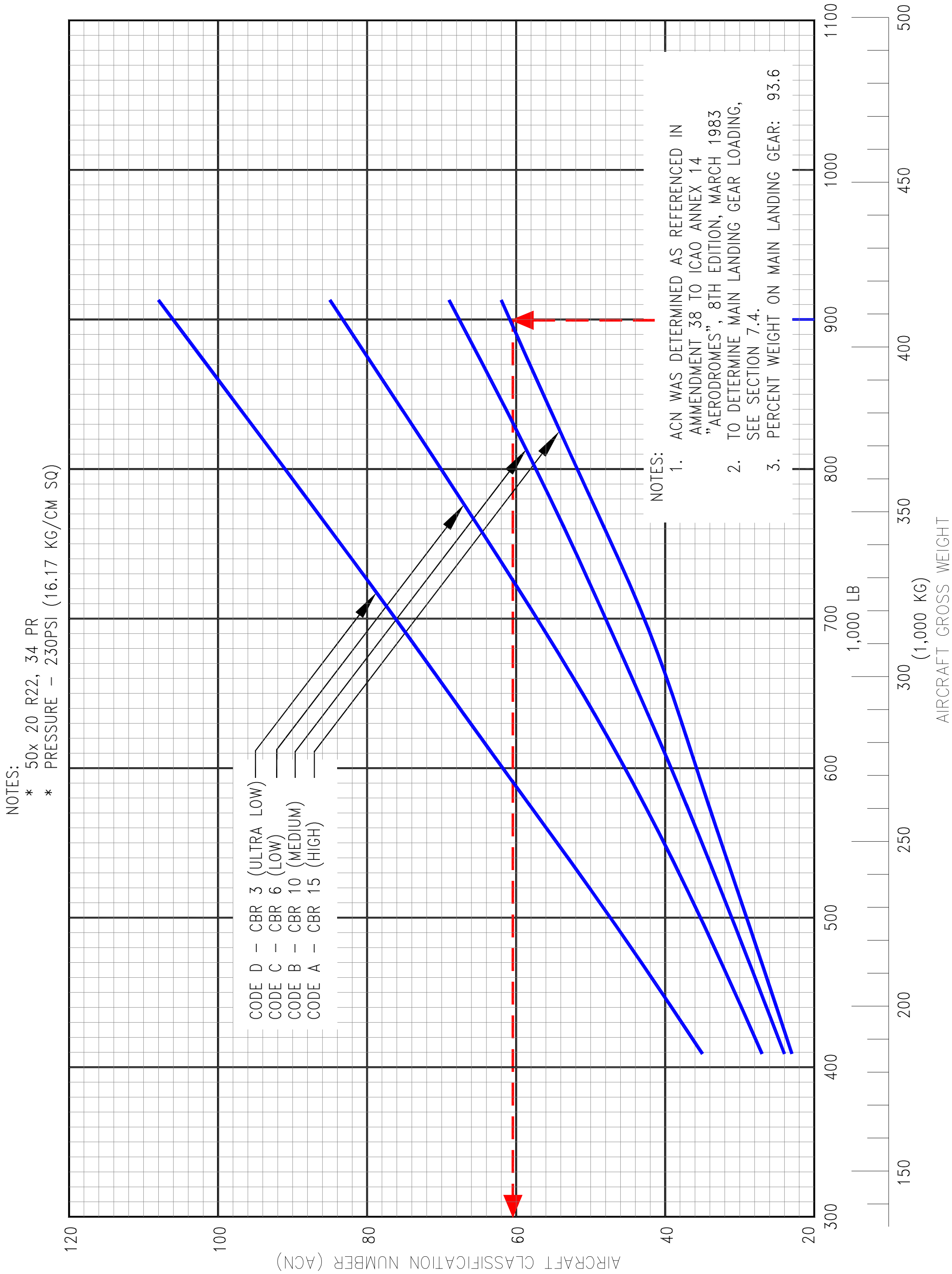
The following table provides ACN data in tabular format similar to the one used by ICAO in the "Aerodrome Design Manual Part 3, Pavements." If the ACN for an intermediate weight between taxi weight and empty fuel weight of the aircraft is required, Figures 7.10.1 through 7.10.4 should be consulted.

				ACN FOR RIGID PAVEMENT SUBGRADES – MN/m^3				ACN FOR FLEXIBLE PAVEMENT SUBGRADES – CBR			
AIRCRAFT TYPE	ALL-UP MASS/ OPERATING MASS EMPTY LB (KG)	LOAD ON ONE MAIN GEAR LEG (%)	TIRE PRESSURE PSI (MPa)	HIGH 150	MEDIUM 80	LOW 40	ULTRA LOW 20	HIGH 15	MEDIUM 10	LOW 6	ULTRA LOW 3
747-400, -400F	877,000(397,800) 364,000(165,107)	23.33	200(1.38)	53 18	62 19	74 22	85 26	58 19	64 20	80 23	102 29
747-400ER, -400 ER FREIGHTER	913,000(414,130) 409,000(185,520)	23.40	230 (1.58)	59 21	69 24	81 27	92 31	62 23	69 24	85 27	108 35

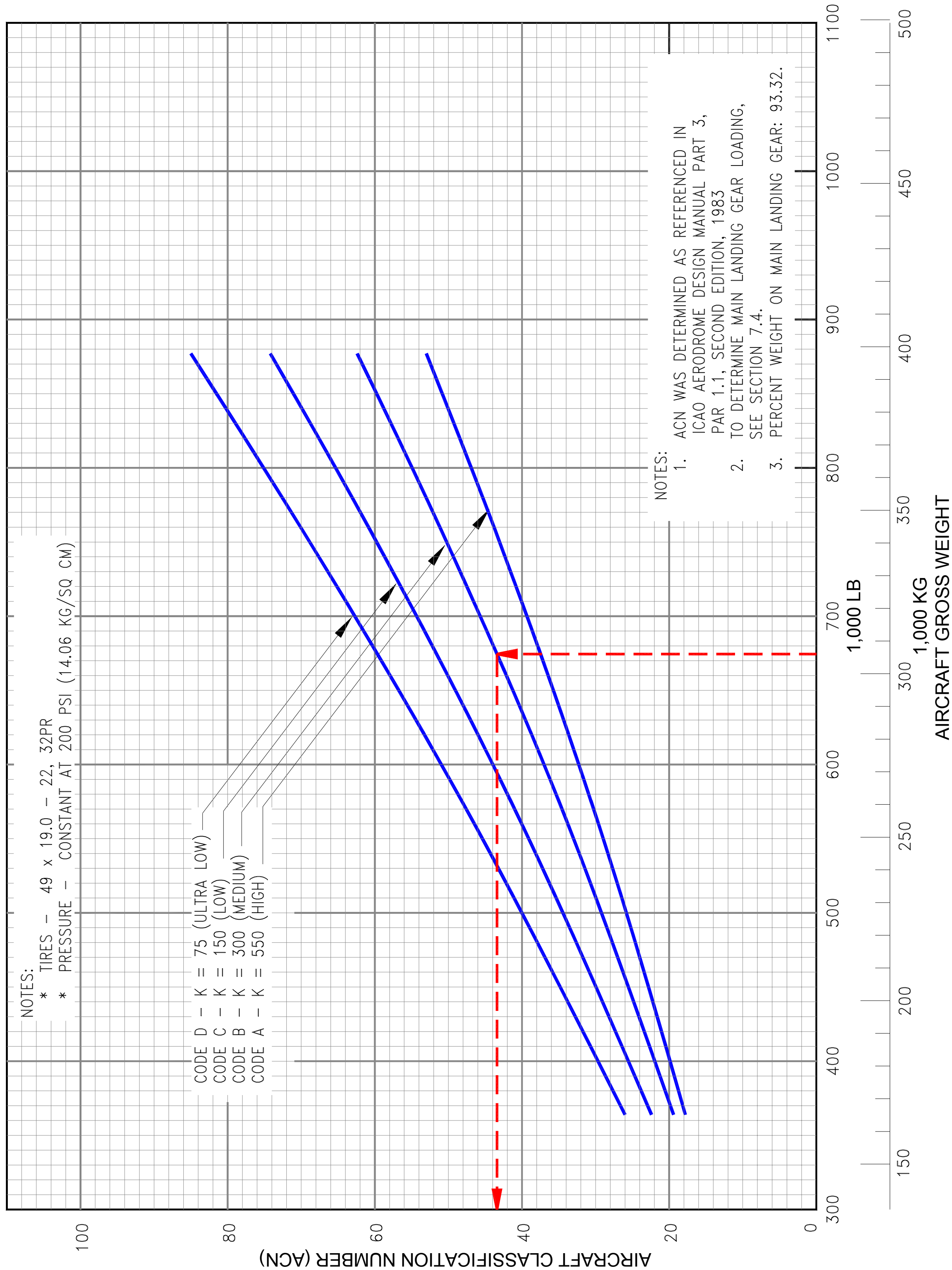


7.10.1 AIRCRAFT CLASSIFICATION NUMBER - FLEXIBLE PAVEMENT

MODEL 747-400, -400 COMBI, -400 DOMESTIC, - 400 FREIGHTER

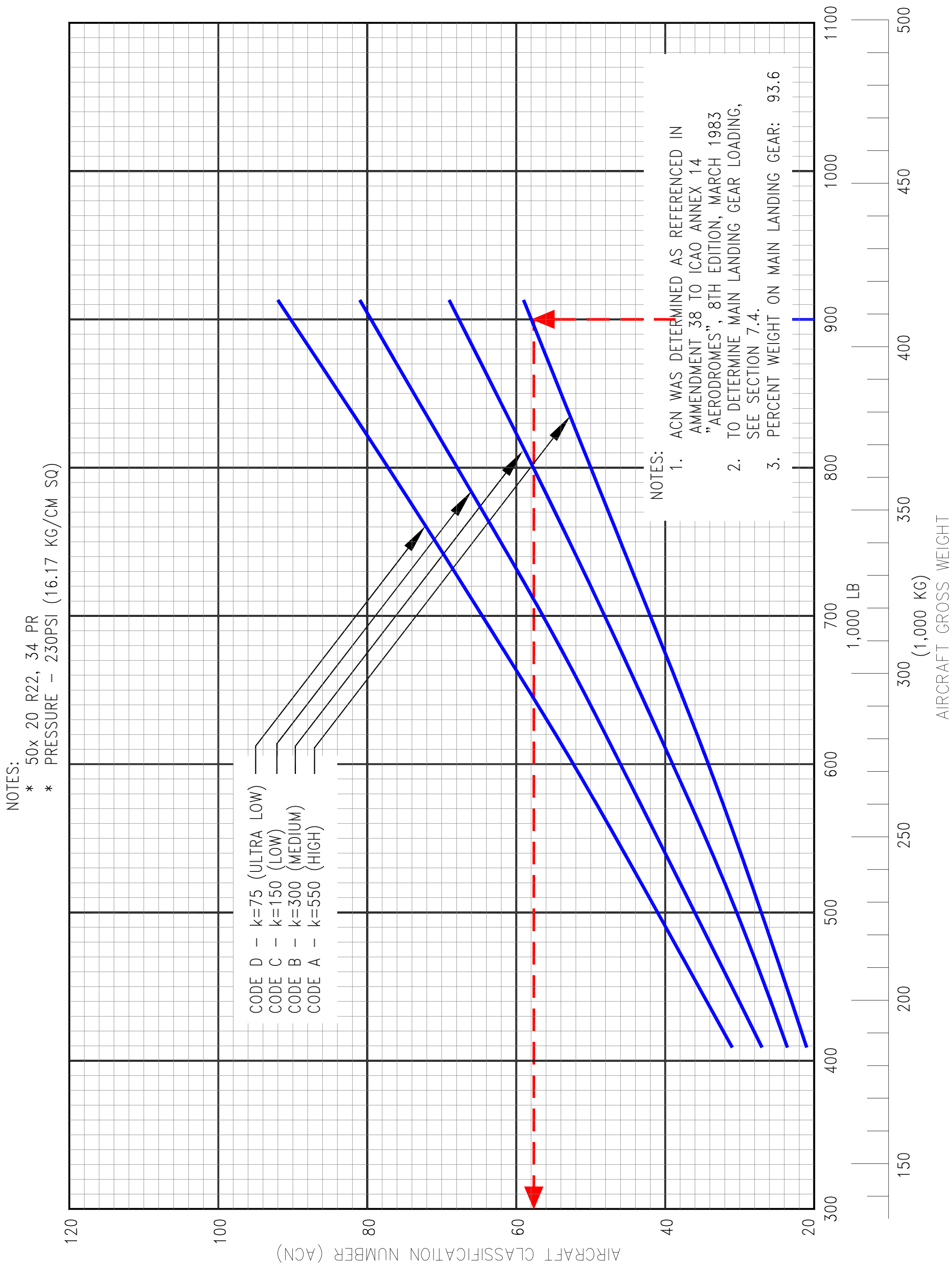


7.10.2 AIRCRAFT CLASSIFICATION NUMBER - FLEXIBLE PAVEMENT
MODEL 747-400ER, -400ER FREIGHTER



7.10.3 AIRCRAFT CLASSIFICATION NUMBER - RIGID PAVEMENT

MODEL 747-400, -400 COMBI, -400 DOMESTIC, - 400 FREIGHTER



7.10.4 AIRCRAFT CLASSIFICATION NUMBER - RIGID PAVEMENT

MODEL 747-400ER, -400ER FREIGHTER